



PROMOTiON

PROGRESS ON MESHED HVDC
OFFSHORE TRANSMISSION
NETWORKS



Mechanical HVDC Circuit Breaker with Active Resonant Current Zero Creation

Mitsubishi Electric Europe

27 th September 2019



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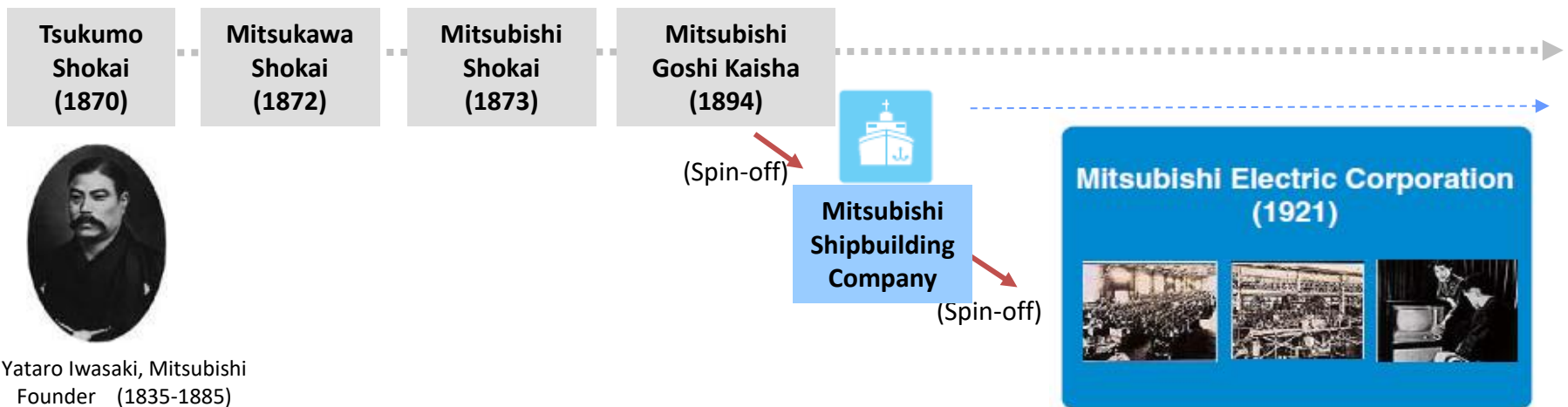
This project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No 691714.

Mitsubishi Companies

- Over 40 Mitsubishi Group companies which share a common heritage
- Each Mitsubishi company now operates independently



Mitsubishi Electric's Origin



T&D Business Organization

North America

Europe

Mid -East

Japan, Asia

MEPPI (US)

- T&D
- SVC/STATCOM
- HVDC

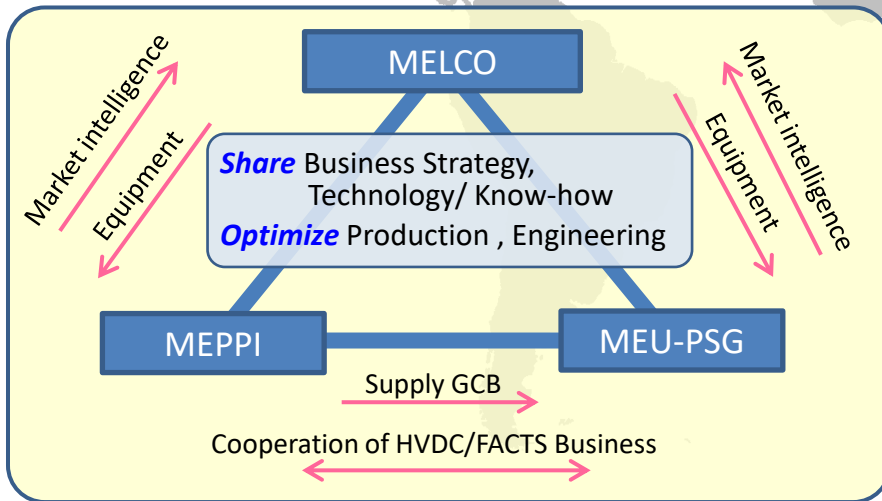
- GCB
- Transformer

MEU - PSG (UK)

- T&D
- SVC/STATCOM
- HVDC

MELCO (Japan)

- GIS
- GCB
- MV/LV SWGR
- Interrupter
- Transformer
- SVC/STATCOM
- HVDC



Legend



Works



Engineering

[MELCO] Mitsubishi Electric Corporation

[MEPPI] Mitsubishi Electric Power Products Inc.

[MEU-PSG] Mitsubishi Electric Europe, Power Systems Group

Confidential

MEU - PSG Experience

Isllington 145kV GIS Substation



Swansea North 420kV GIS Substation



Blyth 400kV Substation - FTK



Chilling 400kV Substation - FTK



HVDC-DIAMOND™



- **50MW Back-Back VSC HVDC Verification Facility – Commissioned in Nov. 2018**

Synchronous Condenser



- **First Synchronous Condenser – 1929**
- **Mitsubishi has supplied > 2,137 large generators**

SVC-DIAMOND™



- **MMC-STATCOM and SVC**
- **More than 12000Mvar installed so far**

GIS/ AIS Substation

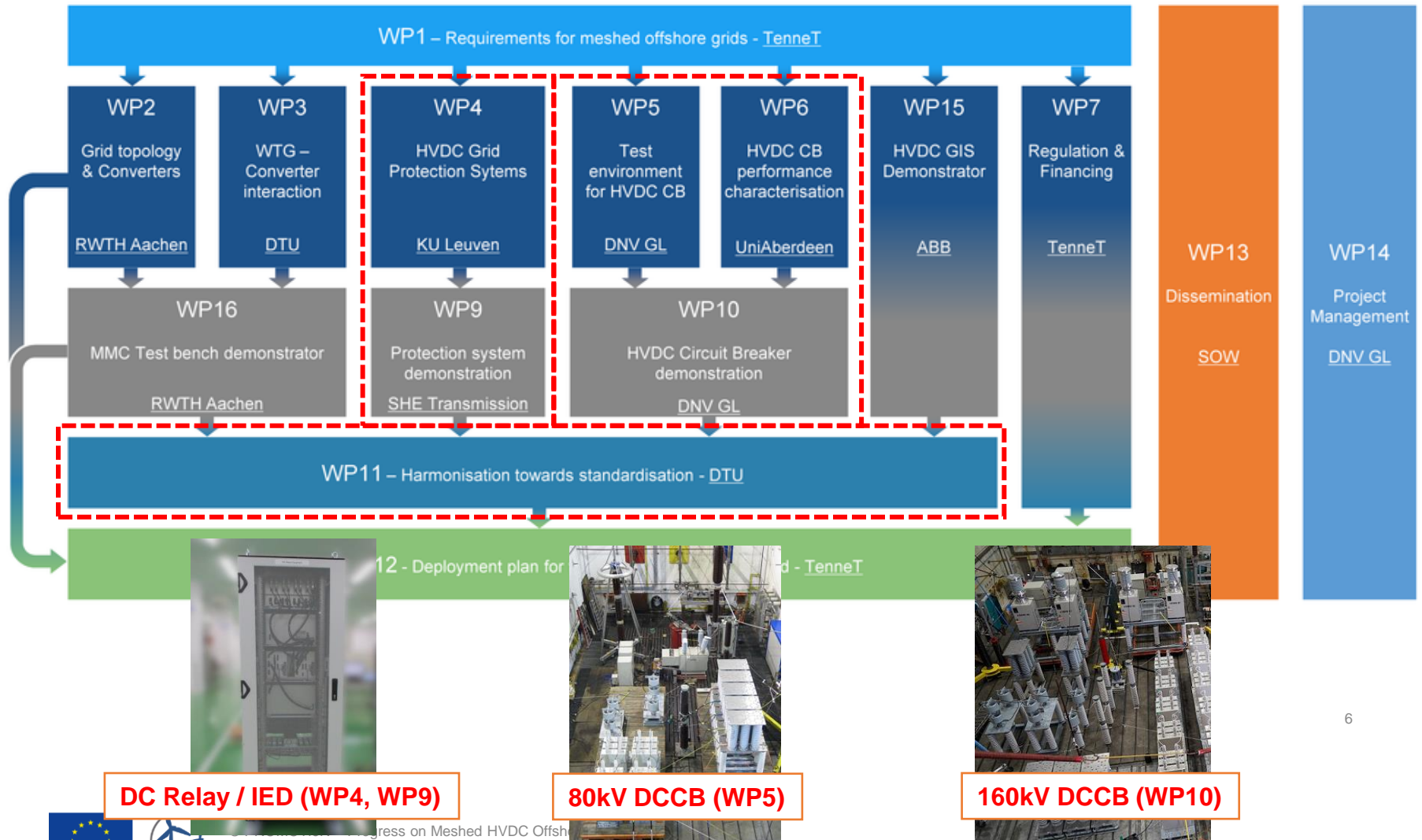


- **35 Years of experience in Europe**

PROMOTion and MEU

PROMOTion – Project organisation

Work packages



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HVDC circuit breaker requirements

■ The requirements for HVDC circuit breakers (no international standards)

HVDC transmission system voltages: 525 kV/ 320 kV

Short-circuit currents: up to 16-20 kA depending on fault current clearing time

Fault current clearing (neutralization) time: 3-8 ms depending on system inductance

MOSA energy dissipation: 20-40 MJ depending on system inductance

Technology: Mechanical DCCB with current injection, Hybrid DCCB

- Rapid fault current clearing after the detection
- Rapid making switch operation for current commutation or current injection
- Long term reliability, Less maintenance works, Economic cost
- Large energy dissipation with multi-columns MOSA units
- Disconnection of residual current through MOSA units
- Rapid auto reclosing for HVDC OHL
- Negligible conduction losses



DCCB Topology

-Mechanical HVDC Circuit Breaker with Active Resonant Current Zero Creation-

Energy Dissipation Branch

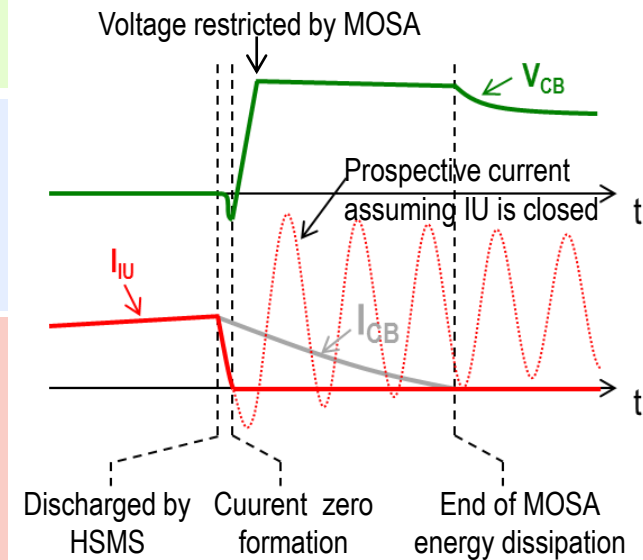
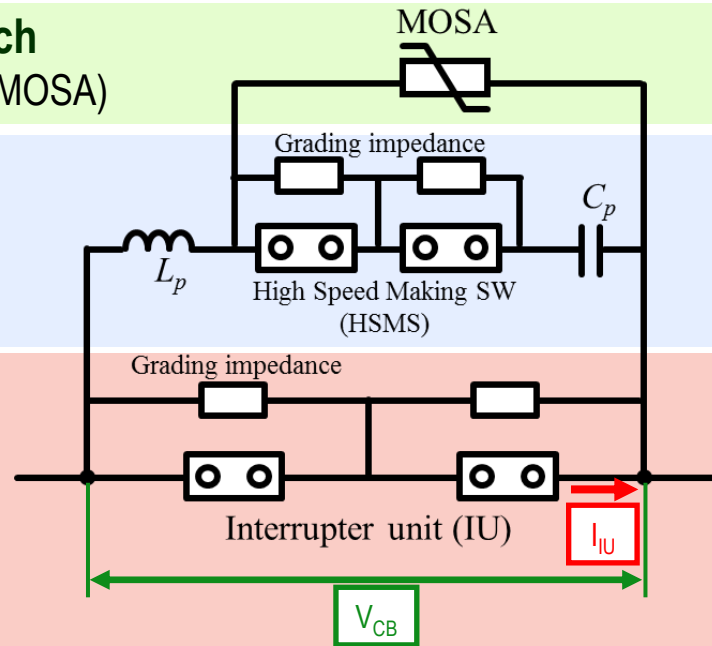
Metal Oxide Surge Arresters (MOSA)

Current Injection Branch

Making switch, Pre-charged capacitor and inductance

Circuit Breaker Branch

Vacuum Interrupter,
Main current carrying circuit



Voltage and current waveforms during current interruption process

Configuration of double break mechanical HVDC circuit breaker

■ Current interruption process

- Vacuum interrupter (VI) is used for the interrupter unit.
- A current zero is created by superimposing high frequency current on DC current (I_{IU}) by discharging the charged capacitor (C_p).
- Current is interrupted at first current zero.

DCCB Topology

-Mechanical HVDC Circuit Breaker with Active Resonant Current Zero Creation-

Energy Dissipation Branch

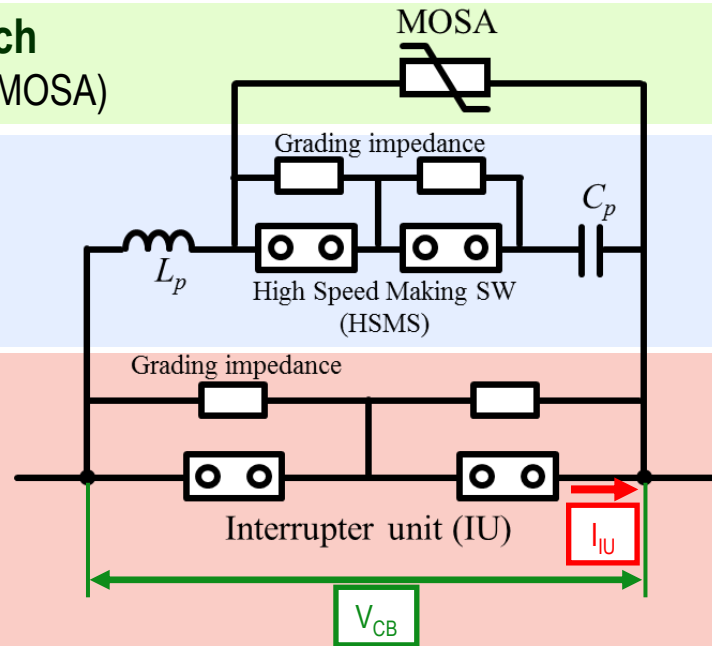
Metal Oxide Surge Arresters (MOSA)

Current Injection Branch

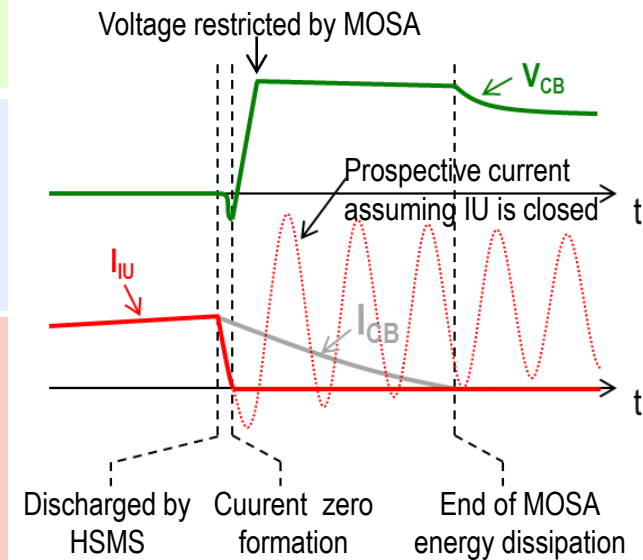
Making switch, Pre-charged capacitor and inductance

Circuit Breaker Branch

Vacuum Interrupter,
Main current carrying circuit



Configuration of double break mechanical HVDC circuit breaker



Voltage and current waveforms during current interruption process

■ MOSA energy dissipation process

- After current interruption, transient interruption voltage (TIV) is imposed on the interrupter.
- TIV is clipped by the MOSA restriction voltage (typically about 1.5 p.u. of the rated voltage in accordance with V-I characteristic) and energy stored in inductive circuit is dissipated by the MOSA.

DCCB Topology

-Mechanical HVDC Circuit Breaker with Active Resonant Current Zero Creation-

Energy Dissipation Branch

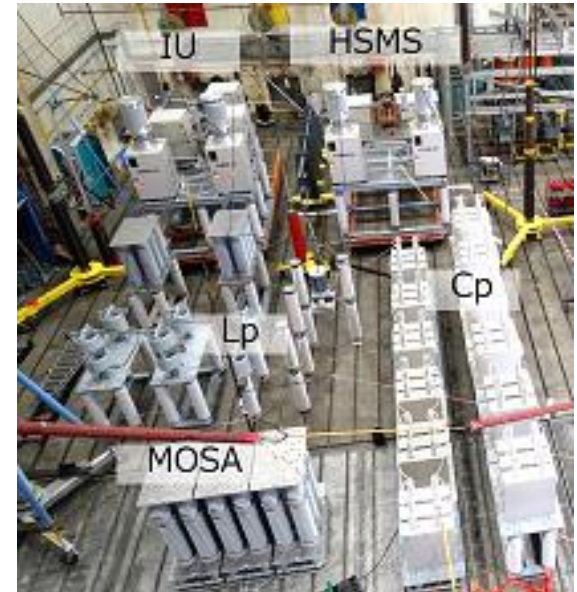
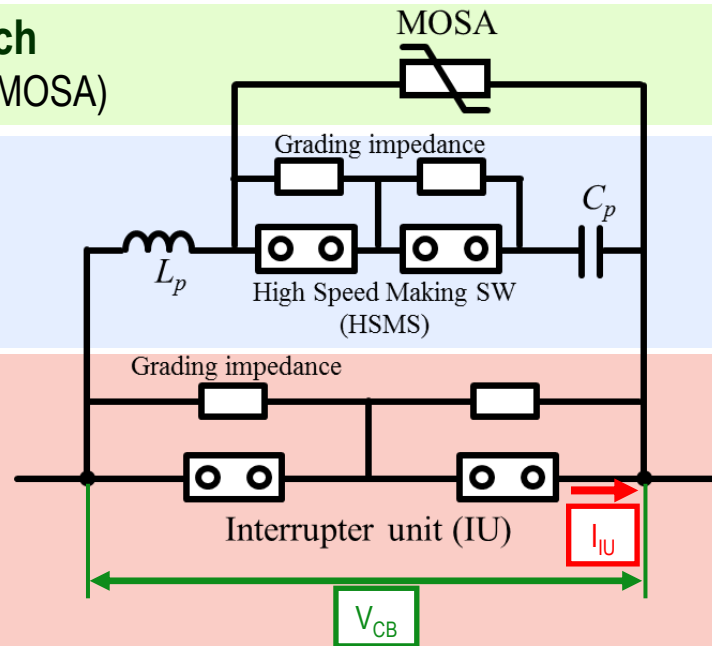
Metal Oxide Surge Arresters (MOSA)

Current Injection Branch

Making switch, Pre-charged capacitor and inductance

Circuit Breaker Branch

Vacuum Interrupter,
Main current carrying circuit



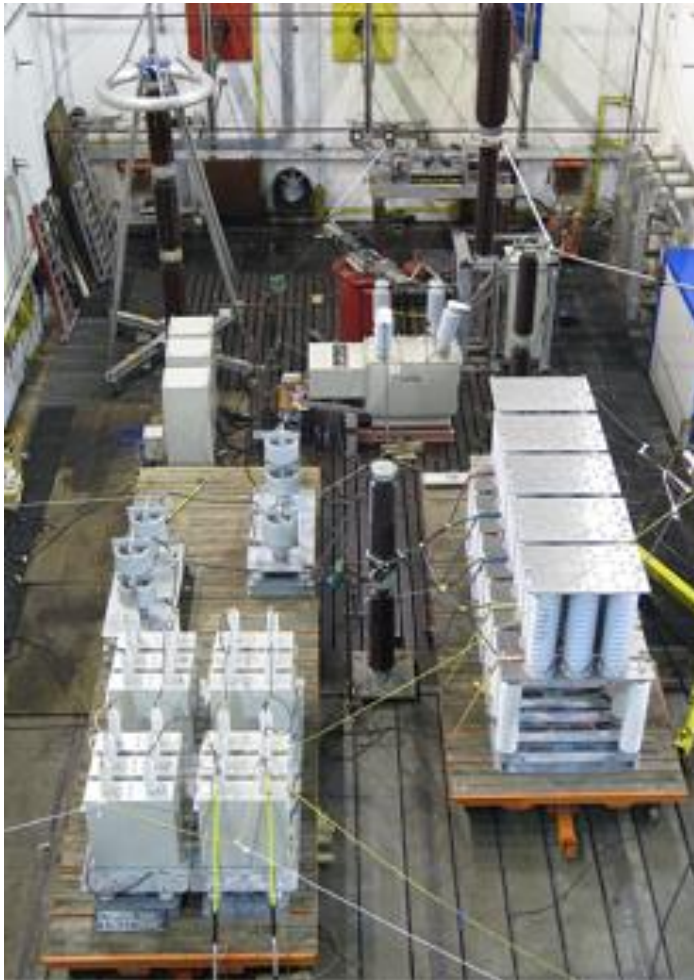
Double break 160 kV mechanical DCCB proto-type setup

Configuration of double break mechanical HVDC circuit breaker

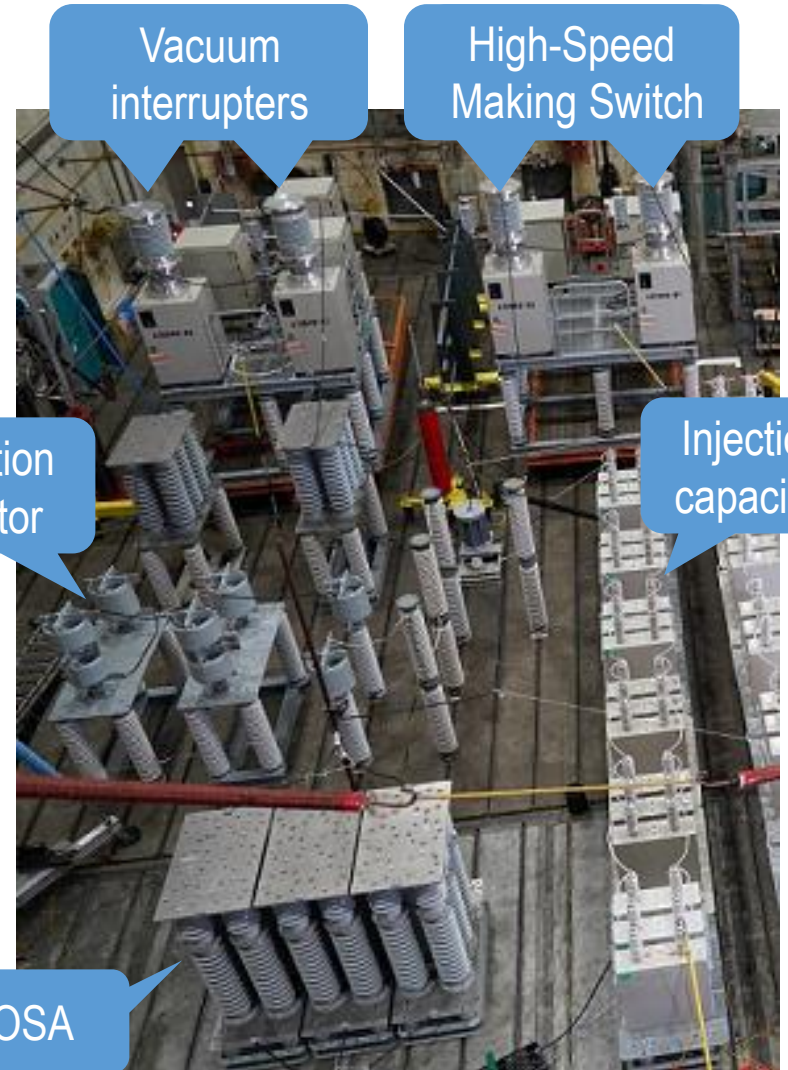
■ MOSA energy dissipation process

- After current interruption, residual current through vacuum interrupter is commutated to the current injection branch, which charges the capacitor.
- The transient interruption voltage (TIV) is clipped by the MOSA restriction voltage (typically about 1.5 p.u. of the rated voltage in accordance with V-I characteristic) and energy stored in inductive circuit is dissipated by the MOSA.

DNV-GL's KEMA High Power Laboratory



**80 kV Unit DCCB testing
August and September, 2017**



**160/200 kV Double break DCCB testing
June, 2019**



Testing conditions of 160/200 kV DCCB demonstration

Test conditions

Items	Conditions
Test method	Reduced power frequency short-circuit generator method
Breaking current	0.2 kA, 2 kA, 16 kA
TIV peak	250 kV
MOSA dissipation energy	4 MJ maximum



Energy Dissipating Requirements

- The energy capacity of MOSA applied to DC circuit breaker is required to cope with **two interruptions** with rated short circuit current (e.g. DC 16 kA).
- Typical MOSA unit is designed with **high homogeneity** multi-columns connected in parallel.



Homogeneous MOSA elements are chosen by an element screening.

Homogeneous MOSA columns are chosen by a column screening

Variation of Residual Voltage: < 0.2%

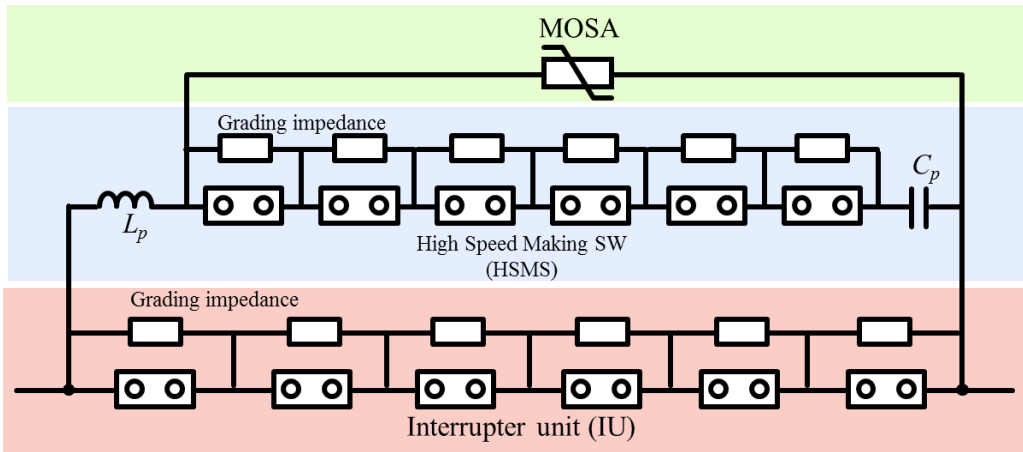
V-I characteristic of a Multi-column MOSA are verified

Typical MOSA energy capacity required for 320 kV DC circuit breakers

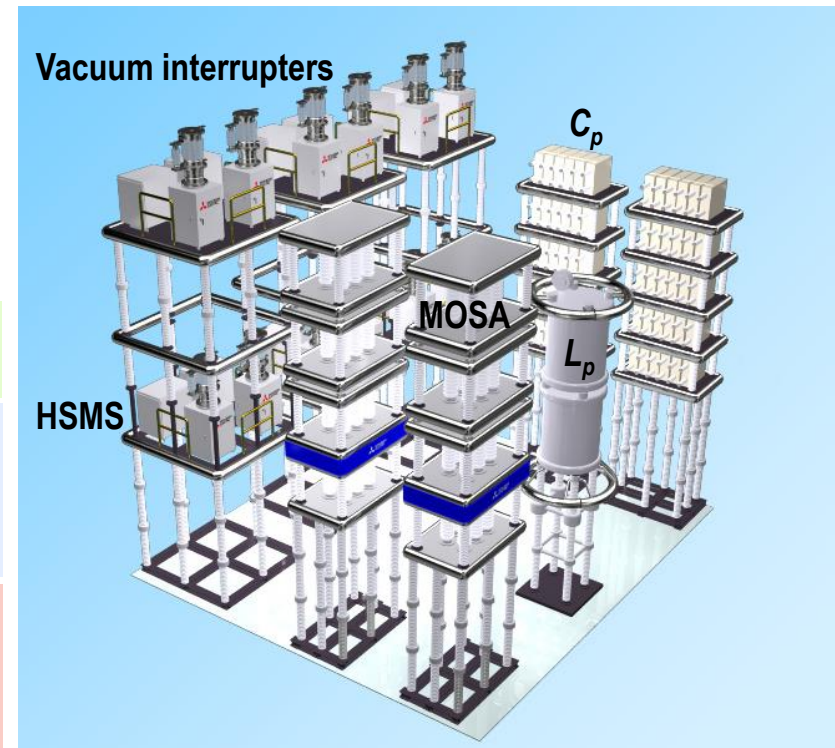
$$E = \frac{1}{2} LI^2 = \frac{1}{2} \times 200 \text{ mH} \times (16 \text{ kA})^2 \approx 24 \text{ MJ}$$

525/600 kV 16 kA DC circuit breaker

- Mechanical HVDC Circuit Breaker with Active Resonant Current Zero Creation -



Configuration of 6 break mechanical DCCB



Conceptual design of 525/600 kV DCCB with 6 VI

- High voltage DCCB can be realized by connecting VI in series.
- The conceptual design shows the 525/600 kV DCCB, connecting six VIs in series.

Summary

- Double break 160/200 kV mechanical DCCB was demonstrated at DNV-GL KEMA HPL lab.
- Interruption test at DCCB voltage of 160 kV, 0.2 ~ 16 kA was interrupted successfully.
- Successfully interrupted bi-directional current of 16 kA at first current zero.
- Temperature rise of each MOSA column was uniform after the interruption test.
- It shows a good result that MOSA column of parallel connection is applicable for HVDC circuit breaker.

Multi-break HVDC circuit breaker with current injection applied with the multi-column well-screening MOSA units as well as the equal voltage division technique can be feasible for 525 /600 kV, 16 kA ratings and above.

Mitsubishi Electric is ready for field installment of HVDC circuit breakers.





Thank You



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