

Control and Stability Analysis of Offshore Meshed HVDC Grids

Modeling HVDC grids as a feedback control system

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Table of contents

1. Introduction
2. Feedback Control System Model and its Benefits
3. Developing Feedback Control System Model for an HVDC Grid
4. Simulation Results
5. Conclusions

Introduction

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- Control paradigm depends on wind farm production

Research Questions Related to DC Grids:

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- Can conventional tools be used for DC grid stability analysis?

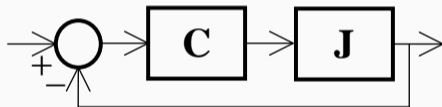
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- more possible questions!

Feedback Control System Model and its Benefits

An appropriate model (a tool) to answer the research questions:

Modeling entire system as a linear, time invariant, multi-input multi-output **Feedback Control System (FCS)**



The FCS model is a basic concept in control engineering!

J and **C** are respectively plant (Jacobian) and controller system model in Laplas domain.

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- The Grid Code Requirements can be taken into account when the limits for the system stability and performance are determined.

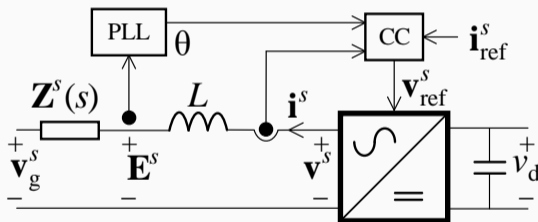
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- An appropriate model for controller design (Many controller design methods are based on the open loop transfer function).
- The Grid Code Requirements can be taken into account when the limits for the system stability and performance are determined.
- The interaction between ac and dc systems, and also between converters can be quantified and qualified.

Example 1: Stability of Current Control Loop of a Grid Connected VSC

A VSC connected to strong DC and AC grids at both sides.

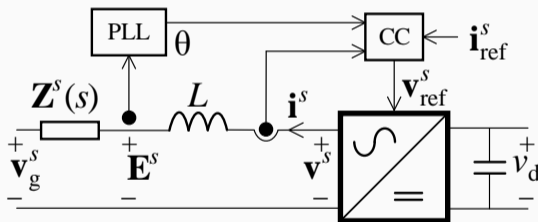
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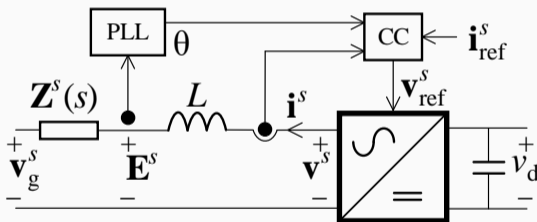
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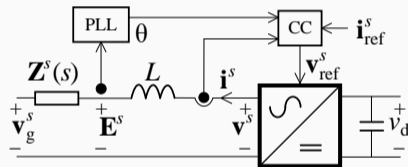
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- Does this control loop ever go to instability?
- If yes, what is the cause?
- And how it can be identified and taken into account in controller design?



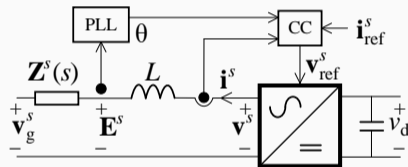
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- System becomes unstable when the controller gain has a large value.



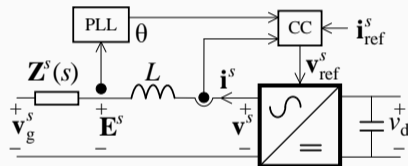
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- System becomes unstable when the controller gain has a large value.
- Transport and sampling delay caused by the PWM process and digital controller sampling/computation can lead to instability [Holmes et al., 2009].



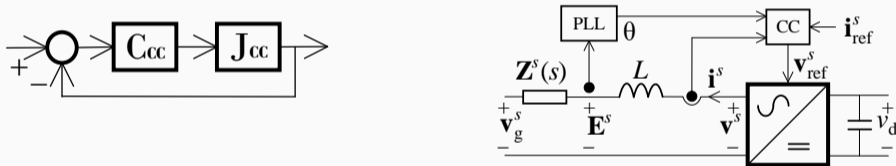
Example 1: Stability of Current Control Loop of a Grid Connected VSC

- System becomes unstable when the controller gain has a large value.
- Transport and sampling delay caused by the PWM process and digital controller sampling/computation can lead to instability [Holmes et al., 2009].
- With modal analysis stability and its cause is not identified.



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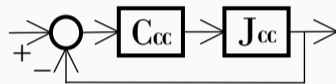
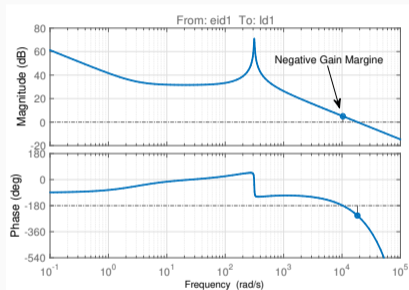
For stability analysis the frequency response of FCS open loop model is used.



J_{CC} is the AC system model and C_{CC} current controller model.

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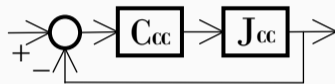
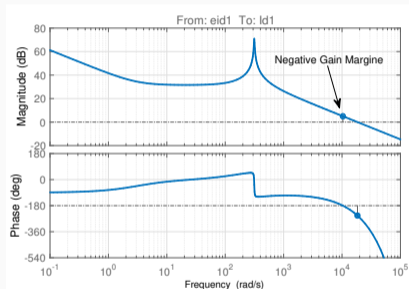
The frequency response of the system indicates that the system is unstable!



- The negative gain margin in open-loop transfer function indicate the instability.

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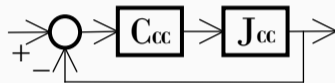
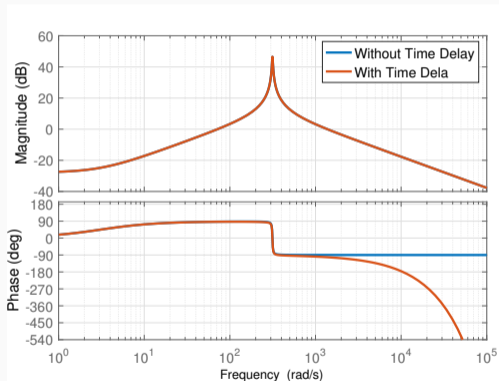
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- The negative gain margin in open-loop transfer function indicate the instability.
- How to detect the cause of instability?

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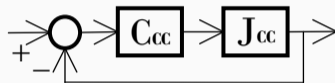
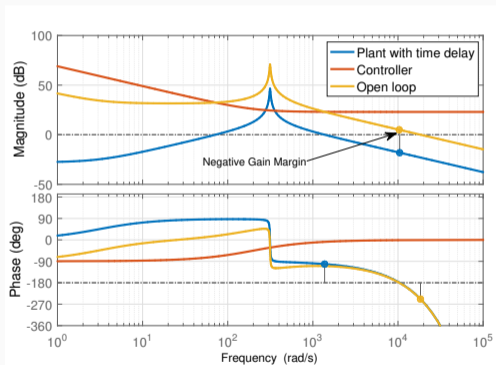
The frequency response of the plant model with and without time delay!



Time delay changes the phase of the plant model, J , at high frequency.

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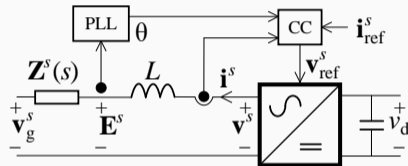
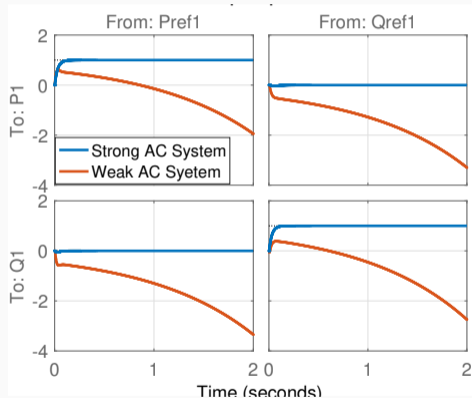
The controller must have low gain at high frequency.



In controller design the time delay must be taken into account!

Example 2: Stability of Power Control Loop of a Weak Grid Connected VSC

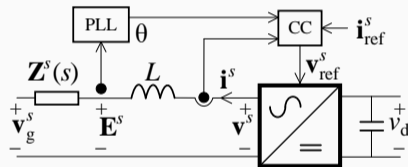
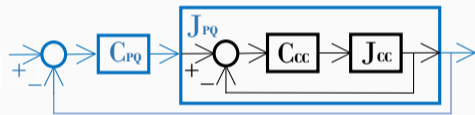
A VSC connected to a weak AC grid.



The system is unstable when AC grid is weak!

Example 2: Stability of Power Control Loop of a Weak Grid Connected VSC

The FCS model for power control loop!

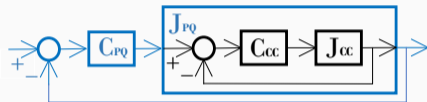
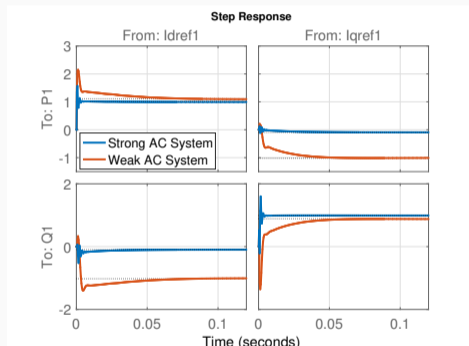


J_{PQ} is the plant model (AC system and current controller model).

C_{PQ} is the power loop controller model (usually a pair of PI controller).

Example 2: Stability of Power Control Loop of a Weak Grid Connected VSC

The accessibility of the plant, \mathbf{J}_{PQ} , model help to understand the cause of instability!

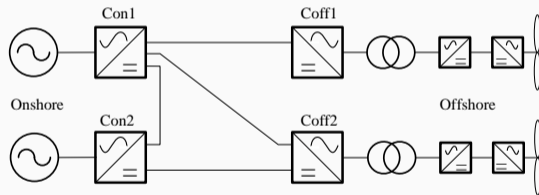


There are severe interactions between P and Q control loops when AC grid is weak.
The plant is ill-condition at low frequencies!

Developing Feedback Control System Model for an HVDC Grid

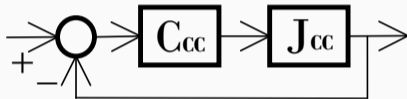
FCS Model of an HVDC Grid:

One of the possible DC grid topologies considered for North Sea



FCS Model of an HVDC Grid:

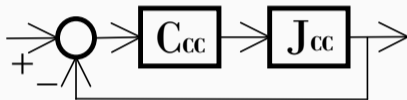
FCS Model for Converters Current Control Loop:



- The model is block-diagonal i.e. DC grid dynamic can be neglected and CC can be design independently for each converter!

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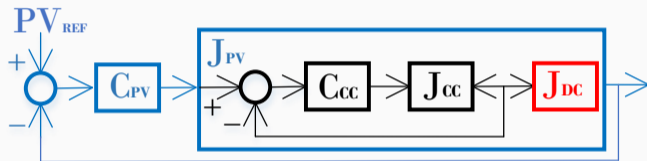
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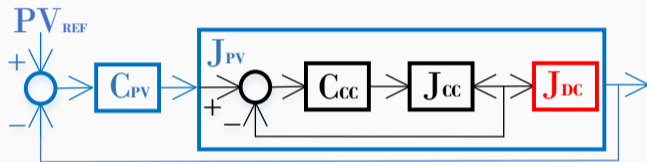
FSC model for Power (Active and Reactive) and Voltage (AC and DC) Control



- The DC grid dynamic, J_{DC} , is included in the plant model, J_{PV} .

FCS Model of an HVDC Grid:

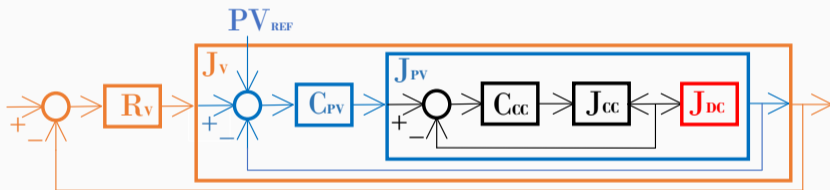
FSC model for Power (Active and Reactive) and Voltage (AC and DC) Control



- The DC grid dynamic, J_{DC} , is included in the plant model, J_{PV} .
- Each AC system is represented by a Thevenin equivalent (detailed model can be regarded of a fast dynamic device like FACTS devices is in nearby).

FCS Model of an HVDC Grid:

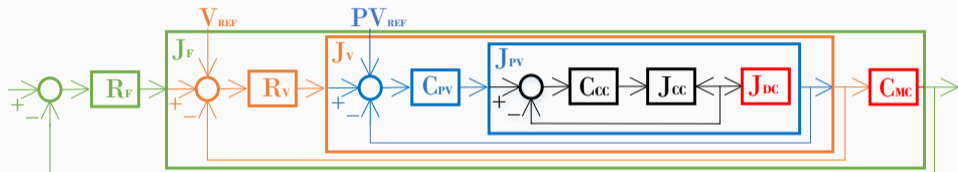
FSC model for Direct Voltage Droop Control



- The direct voltage controller gain, R_v , is the inverse of power-voltage droop!

FCS Model of an HVDC Grid:

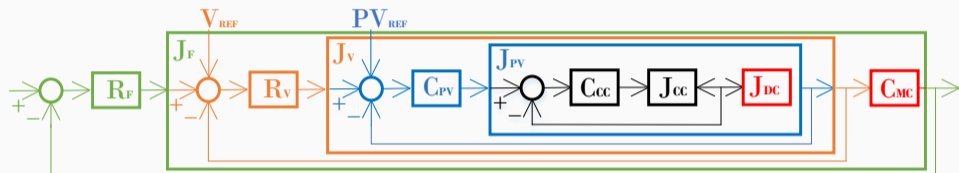
FSC model for Providing Frequency Support to Onshore Grids



- Electromechanical dynamics, C_{MC} , of onshore AC systems are included in the plant model, J_F .

FCS Model of an HVDC Grid:

FSC model for Providing Frequency Support to Onshore Grids



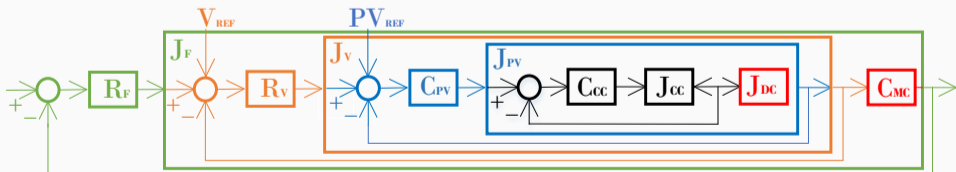
- Electromechanical dynamics, \mathbf{C}_{MC} , of onshore AC systems are included in the plant model, \mathbf{J}_F .
- There are different schemes of implementing frequency support control (with or without communication, converter pairing, etc.).

FCS Model of an HVDC Grid:

Simplification:

When studying a slow dynamic phenomenon, faster dynamic control loops can be simplified. E.g., in frequency support modeling the converter current control loop can be ignored or simplified by a first order dynamic as:

$$\mathbf{I} = \mathbf{T}_{CC} \mathbf{I}_{ref}, \quad \mathbf{T}_{CC} = \frac{\omega_c}{s + \omega_c}, \quad \omega_c \approx 1000 \rightarrow 5000 \text{ rad/sec}$$

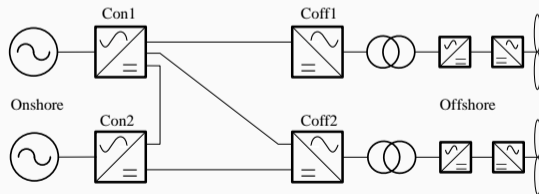


Simulation Results

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Considerations:

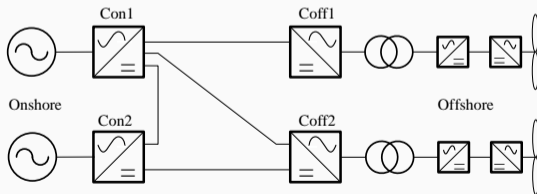
- Dynamics of wind farms are not included (YET) in the FCS model.



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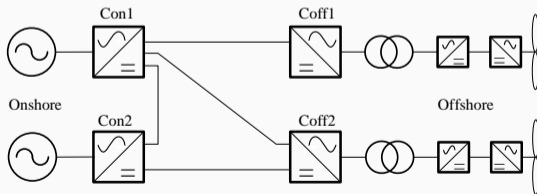
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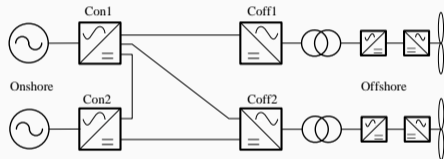
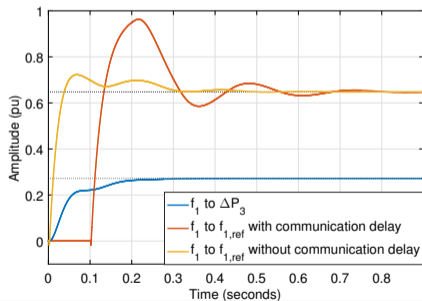
- Dynamics of wind farms are not included (YET) in the FCS model.
- Both of onshore converters participate in direct voltage control.
- Frequency of onshore system one is supported by first offshore wind farm through a communication link.



Simulation Results:

Frequency support from offshore one to onshore one

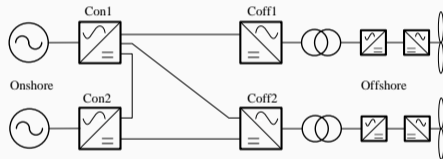
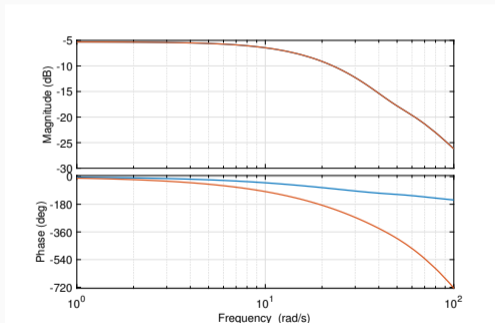
There is 100 ms communication time delay in control loop!



Simulation Results:

Frequency support from offshore one (C3) to onshore one (C1)

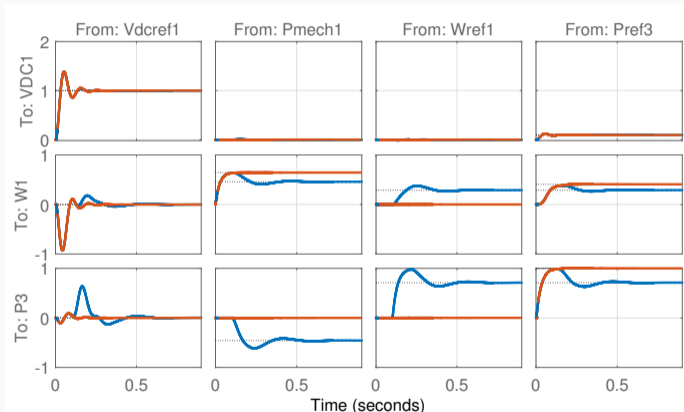
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Simulation Results:

Point-to-point connection between Con.1 and Con.3

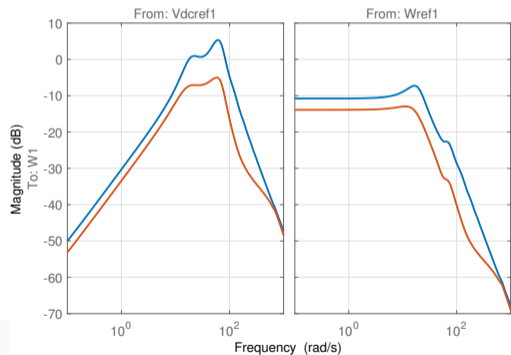
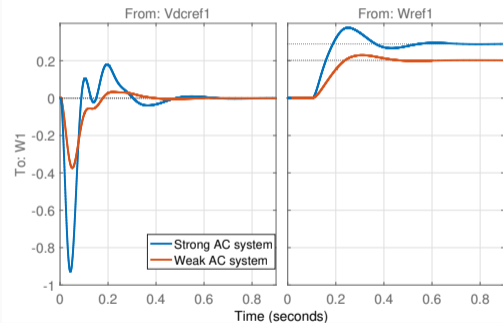
Frequency control creates more interactions between converters. Some overshoots in active power of Con3 must be limited by a proper controllers/limiters.



With frequency control; Without frequency control

Simulation Results:

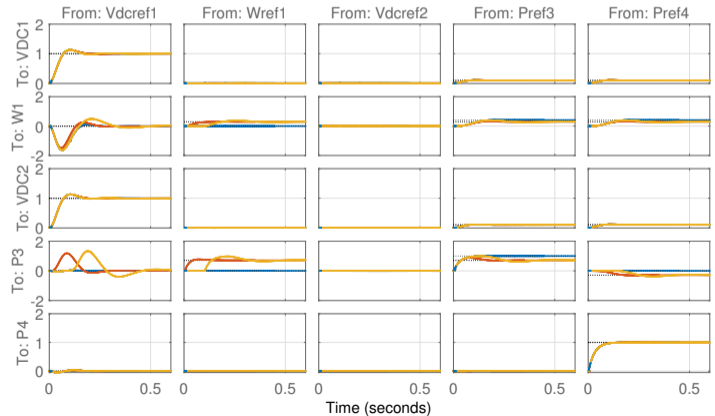
Point-to-point connection between Con.1 and Con.3



Simulation Results:

Meshed HVDC grid with master-slave control: Con.1 in onshore side controls the direct voltage.

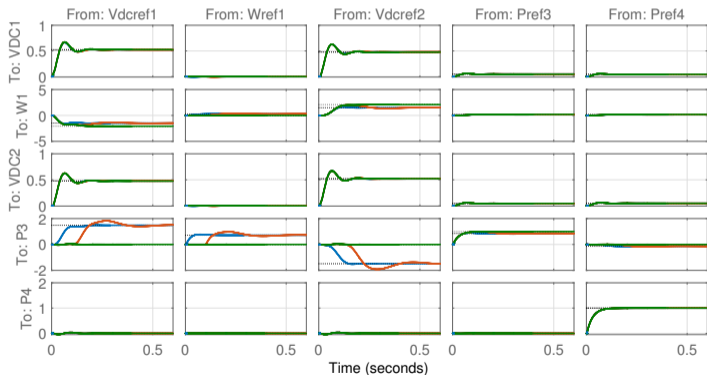
In this control scheme the Con2 and Con4 have not been impacted by frequency control.



Simulation Results:

Meshed HVDC grid with voltage droop control: onshore converters (Con1 and Con2) control the direct voltage.

With communication based frequency control the operation of non-relevant converters is not impacted significantly!



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- Interactions between different inputs and outputs can be quantified.
- Frequency and voltage droop controls create complicated interactions between converters

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More inputs to FCS model:

- Wind turbine model

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Conclusions:

More inputs to FCS model:

- Wind turbine model
- Communication less method for frequency support
- Offshore wind farm with diode rectifier
- Detailed model of AC systems to study power oscillation damping and complicated interactions between AC and DC grids

Questions?

References i

-  Holmes, D. G., Lipo, T. A., McGrath, B. P., and Kong, W. Y. (2009).
Optimized design of stationary frame three phase ac current regulators.
IEEE Transactions on Power Electronics, 24(11):2417–2426.